# McGill University Department of Mechanical Engineering 

## MECH 541 Kinematic Synthesis

Class Test

## OPEN BOOK. ONLY FACULTY STANDARD CALCULATORS ALLOWED

## Date and Time: December 1st, 2009, from 8:35 a.m. to 9:55 a.m.

1. The synthesis of a symmetric gripper based on a planar four-bar linkage, with $k_{2}=k_{3}$ is revisited. This case is known to lead to a $m \times 2$ synthesis matrix $\mathbf{S}$, with a two-dimensional unknown vector $\mathbf{k}=\left[k_{1}, k_{2}\right]^{T}$ and a $m$-dimensional right-hand side vector $\mathbf{b}$. The synthesis of the linkage was conducted for the data given in Table 1, with $\bar{\phi}_{i}$ denoting the prescribed output-angle value, $\phi_{i}$ the generated value. Furthermore, the sensitivity values of the design error $e_{i}$ w.r.t. the generated value $\phi_{i}$ are displayed in the fifth column of the table.

Table 1: Four data points equally spaced along line $\phi=3 \pi / 2-\psi$

| $i$ th point | $\psi_{i}$ | $\bar{\phi}_{i}$ | $\phi_{i}$ | $\mathrm{~d} e_{i} / \mathrm{d} \phi_{i}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 0.5236 | 4.188 | 4.189 | 1.900 |
| 2 | 0.6981 | 4.015 | 4.014 | 1.948 |
| 3 | 0.8727 | 3.840 | 3.840 | 1.956 |
| 4 | 1.047 | 3.667 | 3.665 | 1.885 |

The corresponding synthesis matrix $\mathbf{S}$ and vector $\mathbf{b}$, both computed at the prescribed values of the output angle, along with the least-square approximation of the synthesis equation $\mathbf{S k}=\mathbf{b}$ are given below ${ }^{1}$ :

$$
\mathbf{S}=\left[\begin{array}{cc}
1 & -1.367 \\
1 & -1.408 \\
1 & -1.409 \\
1 & -1.365
\end{array}\right], \quad \mathbf{b}=\left[\begin{array}{c}
-.8666 \\
-.9847 \\
-.9848 \\
-.8670
\end{array}\right], \quad \mathbf{k}=\left[\begin{array}{l}
2.919 \\
2.771
\end{array}\right]
$$

Letting $\mathbf{S}_{g}$ denote the synthesis matrix evaluated at the generated values, this was obtained as

$$
\mathbf{S}_{g}=\left[\begin{array}{ll}
1 & -1.366 \\
1 & -1.409 \\
1 & -1.409 \\
1 & -1.366
\end{array}\right]
$$

(a) $(10 \%)$ Find the structural error $\mathbf{s}$ of the linkage given by $\mathbf{k}$ above, and show that the linkage thus obtained does not minimize $\mathbf{s}$ at the given four-digit precision; moreover,

[^0](b) ( $40 \%$ ) find an improvement to $\mathbf{k}$ that is expected to give a lower structural error, using verbatim the expression displayed in eq.(3.159) with a four-digit precision. Hints:
(i) The product $\mathbf{A}^{T} \mathbf{A}$, with $\mathbf{A}$ of $m \times 2$, is a $2 \times 2$ matrix whose diagonal entries are the Euclidean norms-squared of the corresponding columns of $\mathbf{A}$, its identical off-diagonal entries being given by the scalar product of those two columns.
(ii) The inverse of a $2 \times 2$ matrix $\mathbf{M}$ is ${ }^{2}$
\[

\mathbf{M}^{-1}=\frac{1}{\operatorname{det}(\mathbf{M})}\left[$$
\begin{array}{cc}
m_{22} & -m_{12} \\
-m_{21} & m_{11}
\end{array}
$$\right]
\]

2. Shown in Fig. 1 is a triangular workpiece $R S T$ that will undergo three steps of machining in a flexible manufacturing cell. As this operation will take place for a large batch of workpieces, the manufacturing engineer has decided to use a four-bar linkage to guide the workpiece through the different poses. Space limitations require that the grounded revolute joints have their centres at points $B(-1,1)$ and $B^{\star}(1,1)$.
(a) $(40 \%)$ Compute the centre $A_{0}$ of the floating joint. Hint: it will help speed up the computations if the synthesis equations are expressed in the form $\mathbf{M a}=\mathbf{n}$, where the row $\mathbf{m}_{j}^{T}$ of the $2 \times 2$ matrix $\mathbf{M}$ and the $n_{j}$ entry of $\mathbf{n}$ are functions of $\mathbf{b}, \mathbf{r}_{j}$ and $\mathbf{Q}_{j}$. Hint (ii) of Problem 1 will also be helpful here.
(b) $(10 \%)$ The circular point of the second dyad $B^{\star} A_{0}^{\star}$ was found to be $A_{0}^{\star}(1-\sqrt{2} / 2, \sqrt{2})$. Assuming that the driving link is $B A_{0}$, determine the type of linkage this is, doublecrank, crank-rocker, rocker-crank or double-rocker.


Figure 1: A triangular workpiece to undergo three machining steps in a flexible manufacturing cell, with lengths in m

[^1]
[^0]:    ${ }^{1}$ These values are slightly different from those given in Class Test 1 , as they were computed with additional digits.

[^1]:    ${ }^{2}$ Caveat: the subscripts of the off-diagonal entries of the expression given in eq.(1.8) are flawed; entries should be swapped.

